



LOW VOLTAGE RIDE-THROUGH (LVRT) OF GRID INTERFACED WIND DRIVEN PMSG

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ABSTRACT

In renewable power generation the wind energy has been noted as the most rapidly growing technology; it attracts interest as one of the most cost-effective ways to generate electricity from renewable sources. Wind generation system has potential application for the grid support. The voltage of the direct driven permanent magnet wind generators (PMSG) is variable due to the intermittent nature of the wind energy. Fluctuating voltage and power is of major concern in the converter based grid connected wind generation systems. An inverter is essential for the interfacing of the wind source with the AC network. There are many possible inverter topologies and inverter switching schemes and each one will have its own relative advantages and disadvantages. Variable speed permanent magnet synchronous generators are used for maximum power extraction from the wind energy conversion system. This paper discusses the interconnection issues of these generators to local grid as per prevailing grid standards during healthy and fault conditions. The fault ride-through topology for PMSG has been demonstrated using MATLAB Simulink based simulation.

Keywords: wind, LVRT, power, energy, speed, control, permanent magnet synchronous generator.

1. INTRODUCTION

Because of some challenges such as conventional energy sources consumption, pollution, global climate change and security of energy supply, significant efforts have been made to develop renewable energy sources such as wind energy. Wind power growth with a 20% annual rate has experienced the fastest growth among all renewable energy sources since five years ago. It is predicted that by 2020 up to 12% of the world's electricity will have been supplied by wind power.

In terms of wind power generation technology as a result of numerous technical benefits (higher energy yield, reducing power fluctuations and improving var supply) the modern MW-size wind turbines always use variable speed operation which is achieved by electrical converters. These converters are typically associated with individual generators and they contribute significantly to the costs of wind turbines. The variable speed wind turbine generators such as doubly fed induction generators (DFIGs) and permanent magnet synchronous generators (PMSGs) with primary converters are emerging as the preferred technologies.

As a result of large-scale wind power generation, interconnecting large wind farms to power grids and the relevant influences on the host grids need to be carefully investigated. Wind farms are now required to comply with stringent connection requirements including reactive power support, transient recovery, system stability and voltage/frequency regulation. Further to increase the maximum power extraction the variable speed generators are employed. These variable speed generators necessitate a AC-DC-AC conversion systems. The generator side converter controls the electromagnetic torque and therefore the extracted power while the grid side converter controls both the DC link voltage and the power factor.

Moreover when designing the control strategy it seems that the generator-side converter must control the extracted power as it is located closer to the incoming power. Hence the grid-side converter would control the DC voltage.

Fulfilling the new grid codes constitutes one of the main challenges for the wind power industry. There are ride through requirements. Enhancing the operation of wind turbines in front of the grid faults is mandatory requirement. The wind turbines must stay connected to the grid during grid disturbances. They should continuously feed the reactive power in addition to limited active power. In modern wind turbines the increasing integration of power electronics enables to control the behavior of wind generation system under faulty scenarios [1-5].

The function of an electrical generator is providing a means or energy conversion between the mechanical torque from the wind rotor turbine as the prime mover and the local load or the electric grid. Different types of generators are being used with wind turbines. Small wind turbines are equipped with DC generators of up to a few kilowatts in capacity. Modern wind turbine systems use three phase AC generators [5-11]. The common types of AC generator that are possible candidates in modern wind turbine systems are as follows:

- Squirrel-Cage (SC) rotor Induction Generator (IG);
- Wound-Rotor (WR) Induction Generator;
- Doubly-Fed Induction Generator (DFIG);
- Synchronous Generator (With external field excitation); and
- Permanent Magnet (PM) Synchronous Generator.

For assessing the type of generator in WECS criteria such as operational characteristics, weight of active materials, system cost, maintenance aspects,



reliability and the appropriate type of power electronic converter are used.

Historically induction generator (IG) has been extensively used in commercial wind turbine units. Asynchronous operation of induction generators is considered an advantage for application in wind turbine systems because it provides some degree of flexibility when the wind speed is fluctuating. There are two main types of induction machines: squirrel cage (SC), and wound rotor (WR).

Another category of induction generator is the doubly fed induction generator (DFIG). The DFIG may be based on the squirrel-cage or wound-rotor induction generator.

The induction generator based on Squirrel-Cage rotor (SCIG) is a very popular machine because of its low price, mechanical simplicity, robust structure and resistance against disturbance and vibration. The wound-rotor is suitable for speed control purposes. By changing the rotor resistance the output of the generator can be controlled and also speed control of the generator is possible. Although wound rotor induction generator has the advantage described above it is more expensive than a squirrel-cage rotor.

The Doubly-Fed Induction Generator (DFIG) is a kind of induction machine in which both the stator windings and the rotor windings are connected to the source. The rotating winding is connected to the stationary supply circuits via power electronic converter. The advantage of connecting the converter to the rotor is that variable-speed operation of the turbine is possible with a much smaller and therefore much cheaper converter. The power rating of the converter is often about 1/3 the generator rating [11-14].

Another type of generator that has been proposed for wind turbines in several research articles is synchronous generator. This type of generator has the capability of direct connection (direct-drive) to wind turbines with no gearbox. This advantage is favorable with respect to lifetime and maintenance. Synchronous machines can use either electrically excited or permanent magnet (PM) rotor.

The PM and electrically-excited synchronous generators differ from the induction generator in that the magnetization is provided by a Permanent Magnet pole system or a dc supply on the rotor featuring providing self-excitation property. Self-excitation allows operation at high power factors and high efficiencies for the PM synchronous. It is worth mentioning that induction generators are the most common type of generator use in modern wind turbine systems [15-17].

A comparison between the variable speed wind turbine and the constant speed wind turbine shows that variable speed reduces mechanical stresses: gusts of wind can be absorbed dynamically compensate for torque and power pulsations caused by back pressure of the tower. This backpressure causes noticeable torque pulsations at a rate equal to the turbine rotor speed times the number of rotor blades. The used of a doubly fed induction generator

in WECS with the rotor connected to the electric grid through an AC-AC converter offers the following advantages:

- Only the electric power injected by the rotor needs to be handled by the convert implying a less cost AC-AC converter;
- Improved system efficiency and power factor control can be implemented at lower cost as the converter has to provide only excitation energy.

Hence taking advantage of power electronic advances in recent years WECS equipped with doubly fed induction generator systems for variable speed wind turbine are one of the most efficient configurations for wind energy conversion [11-12].

The advantages of PM machines over electrically excited machines can be summarized as follows according to literatures:

- Higher efficiency and energy yield;
- No additional power supply for the magnet field excitation;
- Improvement in the thermal characteristics of the PM machine due to the absence of the field losses;
- Higher reliability due to the absence of mechanical components such as slip rings; and
- Lighter and therefore higher power to weight ratio.

However, PM machines have some disadvantages, which can be summarized as follows:

- High cost of PM material;
- Difficulties to handle in manufacture; and
- Demagnetization of PM at high temperature.

In the recent years the use of PM is increasing than before because the performance of PM is improving and the cost of PM is decreasing. The trends make PM machines with a full-scale power converter more attractive for direct-drive wind turbines. In addition to that the cost of power electronics is also decreasing the variable speed direct-drive PM machines with a full-scale power converter become more and more popular for offshore wind powers. On the other hand variable speed concepts with a full-scale power converter and a single- or multiple-stage gearbox drive train may be interesting solutions not only in respect to the annual energy yield per cost but also in respect to the total weight. For example the market interest of PMSG system with a multiple-stage gearbox or a single-stage gearbox is increasing. [15-18]

In this paper, first, the grid connections requirements are listed as per IEEE standards. The system modeling for ride-through capability of the PMSG during fault condition is presented. Finally, the MATLAB Simulink based is used to validate the proposed ride-through topology.



2. INTERCONNECTION WITH ELECTRIC POWER SYSTEMS

Distributed resources connected with electric power systems are presented in Figure-1 as typical configurations. The distributed resources include wind, small hydro, micro- turbines, solar photo-voltaic and solar thermal etc. These resources are to be connected to the low voltage power distribution system. The major interconnection requirements for distributed resources can be summarized in the following three categories: general specifications, safety and protection and power quality [1-3].

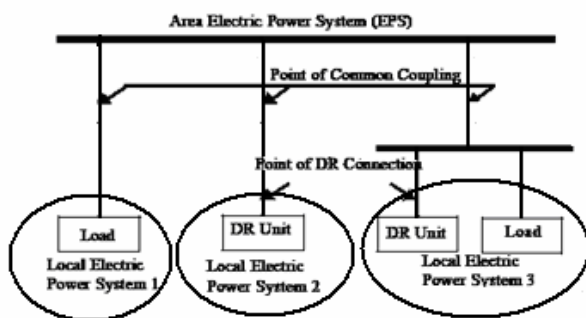


Figure-1. Distributed resources connected to a power system.

3. WIND TURBINE TECHNOLOGIES AND GRID REQUIREMENTS

In this Section a brief review is presented of wind turbine technology aspects, associated with grid code compliance. Wind turbines are generally divided in two main technological categories:

- a) Constant speed wind turbines which are equipped with squirrel cage induction generators directly connected to the grid. The rotational speed of the rotor is practically fixed since they operate at a slip around 1%. Since the induction machine absorbs reactive power from the grid so the connection of compensating capacitor banks at the wind turbine (or wind farm) terminals is necessary. Their aerodynamic control is based on stall active stall or pitch control. A variation of this scheme utilizes a wound rotor induction generator and electronically controlled external resistors to the rotor terminals permitting a variation of speed (typically up to 10% above synchronous).
- b) Variable speed wind turbines the rotor speed of which varies significantly according to the prevailing wind conditions. Two major types are available: The first is utilizes a Doubly-Fed Induction Generator (DFIG) and a rotor converter cascade of reduced rating while the second employs a synchronous or induction generator the stator of which is interfaced to the grid via a full-power converter.

In case of DFIGs the generator's stator is directly connected to the grid while the rotor is connected through a cascade of two voltage source converters (rectifier-inverter, connected back-to-back). Wind turbines with full converter use either a synchronous or an asynchronous generator, whose stator is connected to the grid via an AC/DC/AC converter cascade. In this case, the converter handles the total generator power to the grid and therefore no size economies are possible.

The latest grid codes require that wind farms must remain in operation during severe grid disturbances ensure fast restoration of active power to the prefault levels as soon as the fault is cleared and in certain cases produce reactive current in order to support grid voltage during disturbances. Depending on their type and technology the wind turbines can fulfill these requirements to different degrees as explained in the following. Starting with constant speed wind turbines, their low voltage behavior is dominated by the presence of the grid-connected induction generator. In the event of a voltage dip, the generator torque reduces considerably (roughly by the square of its terminal voltage) resulting in the acceleration of the rotor which may result in rotor instability unless the voltage is restored fast or the accelerating mechanical torque is rapidly reduced. Further the operation of the machine at increased slip values results in increased reactive power absorption particularly after fault clearance and partial restoration of the system voltage. This effectively prevents fast voltage recovery and may affect other neighboring generators whose terminal voltage remains depressed. Since the dynamic behavior of the induction generator itself cannot be improved the measures that can be taken in order to enhance the fault ride-through capabilities of constant speed wind turbines are the following:

- Improvement in the response of the wind turbine aerodynamic control system in order to perform fast limitation of the accelerating mechanical torque to prevent rotor overspeed. Physical limitations of the blades and the pitch regulation mechanism impose a limit on the effectiveness of such an approach.
- Supply of reactive power through static compensation devices at the wind turbine or wind farm terminals such as SVCs or STATCOMs. These devices would provide high amounts of reactive power during faults to effectively support the terminal voltage and therefore limit the magnitude of the voltage dip experienced by the wind turbines. Nevertheless FACTS are complicated and costly devices, while there is an obvious limitation to the voltage correction they can achieve particularly in the event of nearby system faults.

Variable speed wind turbines on the other hand present the distinct advantages of direct generator torque and reactive current control and the possibility to endure



large rotor speed variations without stability implications. For this reason grid disturbances affect much less their operation and generally speaking they are capable of meeting stringent requirements.

In case of voltage disturbances the rotor over speed becomes an issue of much smaller significance, since a limited increase of speed is possible (e.g. 10-15% above rated) the rotor inertia acting as an energy buffer for the surplus accelerating power until the pitch regulation becomes effective. In case of severe voltage dips an energy surplus may occur in the electrical part potentially leading to dc over voltages. This is dealt with by proper redesign of the converter controllers for increase of the local energy storage capacity (e.g. capacitor size) or even by providing local power dissipation means.

However even with variable speed wind turbines there still exist LVRT issues affecting their response. In the case of DFIG wind turbines the direct connection of the generator stator to the grid inevitably results in severe transients in case of large grid disturbances. Hence the stator contributes a high initial short circuit current while large currents and voltages are also induced in the rotor windings as a consequence of the fundamental flux linkage dynamics of the generator. Furthermore the depressed terminal voltage reduces accordingly the power output of the grid side rotor converter leading to an increase of the dc bus capacitor voltage. To protect the power converters from over voltages and over currents DFIGs are always equipped with a device known as a crowbar that short circuit the rotor terminals as soon as such situations are detected. Once the crowbar is activated the DFIG behaves like a conventional induction machine i.e. control is lost over the generator. Notably crowbar activation is possible not only at the instant of a voltage depression but also in case of abrupt voltage recovery after clearance of a fault. Conceptually two crowbar options are available:

- The passive crowbar utilizing a diode rectifier or a pair of antiparallel thyristors to short the rotor terminals. The disadvantage of this option is the lack of control on the deactivation of the crowbar leading to sustained operation with short-circuited rotor.
- The active crowbar that uses IGBT switches to short the rotor. This enhances considerably the operation of the device with a faster elimination of the rotor transients (typically within 100 ms) and therefore faster regain of control. After deactivation of the crowbar full controllability over the wind turbine behavior is resumed.

Hence although voltage dips inevitably cause torque and power transients in the DFIG wind turbine which excite the rotor crowbar protection for a limited time interval the various implementations of the active crowbar can improve the stability of the wind turbine and its response to sudden voltage changes.

Variable speed wind turbines with full power converters present the distinct advantage that the converter

totally decouples the generator from the grid. Hence grid disturbances have no direct effect on the generator whose current and torque variations during voltage dips are much lower compared to the DFIG and the respective transients fade out faster [6-9]. From the point of view of the reactive output power the grid side converter has the ability to produce reactive current during the voltage dip upto its rated current. Notably this wind turbine type may exhibit better voltage control capabilities even than conventional synchronous generators.

Another notable advantage of this type against the DFIG-based wind turbines is related with the behavior of the latter in case of unbalanced disturbances. In such situations the low negative sequence impedance of the induction generator may give rise to large rotor currents whose frequency lies outside the controllers bandwidth resulting in the activation of the crowbar (or the disconnection of the stator) until the disturbance is cleared. Wind turbines can control their active power output by pitch control while variable speed wind turbines have the additional capability for such control via variation of their rotor speed. Hence power curtailment, ramp rate limitations and contribution to frequency regulation is possible even for constant speed machines. In the latter case however the grid frequency is directly related to the generator slip and hence a change in frequency will transiently affect the active power produced by the wind turbine. In the case of variable speed machines on the other hand the generator power is directly controlled and therefore their primary frequency response is entirely adjustable by proper design of the control systems.

4. FAULT RIDE THROUGH REQUIREMENTS

The large increase in the installed wind capacity in transmission systems necessitates that wind generation remains in operation in the event of network disturbances. For this reason grid codes issued during the last years invariably demand that wind farms (especially those connected to HV grids) must withstand voltage dips to a certain percentage of the nominal voltage (down to 0% in some cases) and for a specified duration. Such requirements are known as Fault Ride through (FRT) or Low Voltage Ride through (LVRT) and they are described by a voltage vs. time characteristic denoting the minimum required immunity of the wind power station. The LVRT requirements also include fast active and reactive power restoration to the prefault values after the system voltage returns to normal operation levels. Some codes impose increased reactive power generation by the wind turbines during the disturbance in order to provide voltage support a requirement that resembles the behavior of conventional synchronous generators in over-excited operation. The requirements depend on the specific characteristics of each power system and the protection employed and they deviate significantly from each other.

The required fault behavior of a wind farm can be summarized into four requirements:



- For system faults that last up to 140 ms the wind farm has to remain connected to the network. For supergrid voltage dips of duration greater than 140 ms the wind farm has to remain connected to the system for any dip-duration on or above the heavy black line shown in Figure-2.
- During system faults and voltage sags a wind farm has to supply maximum reactive current to the Grid System without exceeding the transient rating of the plant.
- For system faults that last up to 140ms upon the restoration of voltage to 90% of nominal a wind farm has to supply active power to at least 90% of its pre-fault value within 0.5 sec. For voltage dips of duration greater than 140 ms a wind farm has to supply active power to at least 90% of its pre-fault value within 1 sec of restoration of voltage to 90% of nominal.
- During voltage dips lasting more than 140ms the active power output of a wind farm has to be retained at least in proportion to the retained balanced supergrid voltage [8,9].

It should be noted that in cases where less than 5% of the turbines are running or under very high wind speed conditions where more than 50% of the turbines have been shut down a wind farm is permitted to trip.

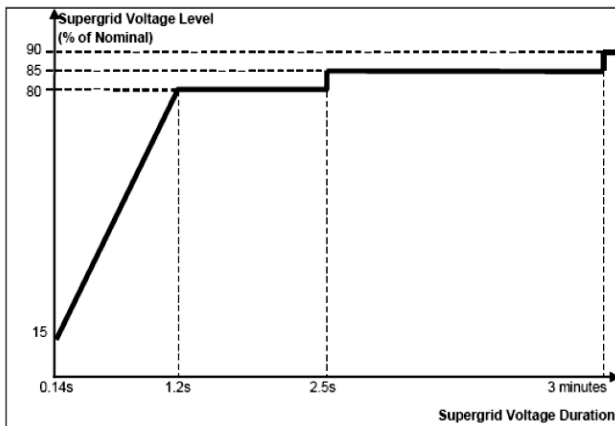


Figure-2. Required ride through capability of wind farms for super grid voltage dips of duration greater than 140ms.

5. VARIOUS RIDE THROUGH TOPOLOGIES FOR GRID CONNECTED VARIABLE SPEED PMSG

Variable speed use is good for extracting more prime mover power as in wind turbine or for providing optimum efficiency for the prime mover by increasing its speed with power. Variable speed also allows for a more flexible generator system. For wind turbines a battery may be added to store the extra wind energy that is not momentarily needed for the existing loads or local power grids [13-16]. There are three main ways to handle the necessity of constant DC link voltage at variable speed:

- a) PMSG with diode rectifier and DC-DC chopper as shown in Figure-3;
- b) PMSG with rectifier and DC-DC boost-converter as shown in Figure- 4; and
- c) PMSG with PWM rectifier with battery for storing the extra wind energy as shown in Figure-5.

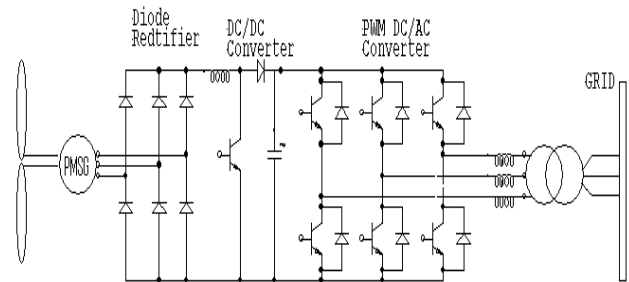


Figure-3. PMSG with diode rectifier and DC-DC chopper.

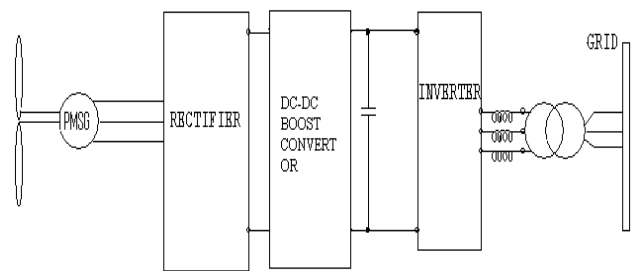


Figure-4. PMSG with rectifier and DC-DC Boost converter.

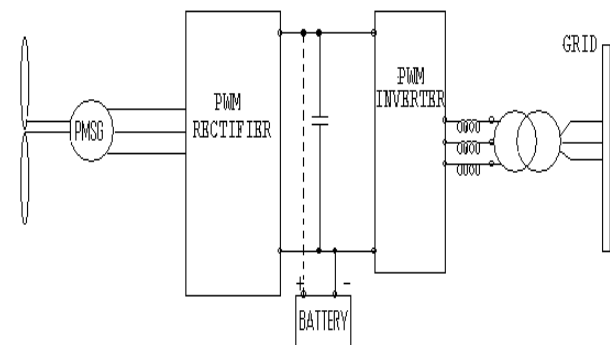


Figure-5. PMSG with PWM rectifier with battery for storing the extra wind energy.

6. MATLAB SIMULATION OF THE PROPOSED TOPOLOGY

The proposed topology is shown in Figure-6 and subsystem in Figure-7. The matlab simulink tool box simpower is used for getting the required results.



7. MODELING OF PROPOSED SYSTEM

This section includes modeling of PMSG, Excitation system, wind turbine and control scheme etc. The relevant mathematical analysis is illustrated as follows.

A. Modeling of Permanent Magnet Synchronous Machine

The permanent magnet synchronous machine block operates in generating or motoring modes. The operating mode is dictated by the sign of the mechanical power (positive for generating, negative for motoring). The electrical part of the machine is represented by a sixth-order state-space model. The model takes into account the dynamics of the stator and damper windings. The equivalent circuit of the model is represented in the rotor reference frame (d-q frame). The following equations are used to express the model of the PMSG as:

$$V_d = R_s i_d + p\phi_d - w_r \phi_q \quad (1)$$

$$V_q = R_s i_q + p\phi_q + w_r \phi_d \quad (2)$$

$$V'_{fd} = R'_{fd} i'_{fd} + p\phi'_{fd} \quad (3)$$

$$V'_{kd} = R'_{kd} i'_{kd} + p\phi'_{kd} \quad (4)$$

$$V'_{kq1} = R'_{kq1} i'_{kq1} + p\phi'_{kq1} \quad (5)$$

$$V'_{kq2} = R'_{kq2} i'_{kq2} + p\phi'_{kq2} \quad (6)$$

$$\text{Where } \phi_d = L_D i_d + L_{md} (i'_{fd} + i'_{kd}) \quad (7)$$

$$\phi_q = L_q i_q + L_{mq} i'_{kq} \quad (8)$$

$$\phi'_{FD} = L'_{fd} i'_{fd} + L_{md} (i_d + i'_{kd}) \quad (9)$$

$$\phi'_{KD} = L'_{kd} i'_{kd} + L_{md} (i_d + i'_{fd}) \quad (10)$$

$$\phi'_{kq2} = L'_{kq2} i'_{kq2} + L_{mq} i_q \quad (11)$$

Where the subscripts used are defined as: d, q: d and q axis quantity, r, s: Rotor and stator quantity, l, m: Leakage and magnetizing inductance, f, k: Field and damper winding quantity. R_s represents stator resistance, L_{ls} stator leakage inductance, L_{md} and L_{mq} represent d-axis and q-axis magnetizing inductances. R'_f denotes field resistance and L_{lfd} leakage inductance both referred to the stator. Damper d-axis resistance R'_{kd} and leakage inductance L_{lkd} , Damper q-axis resistance R'_{kq1} and leakage inductance L_{lkq1} and the q-axis resistance R'_{kq2} and leakage inductance L_{lkq2} . All these values are referred to the stator. All rotor parameters and electrical quantities are viewed from the stator and are identified by primed variables. The simplified synchronous machine block implements the mechanical system described by:

$$\Delta w(t) = \int (T_m - T_e) dt / (2H) - K_d \Delta w(t) \quad (12)$$

$$W(t) = \Delta w(t) + w_o \quad (13)$$

B. Excitation system

The excitation system block is a Simulink system implementing an IEEE Type I synchronous machine voltage regulator combined to an exciter. The basic elements that form the excitation system block are the voltage regulator and the exciter. The exciter is represented by the following transfer function between the exciter voltage V_{fd} and the regulator's output E_f .

$$V_{fd}/E_f = 1/(K_e + sT_e) \quad (14)$$

Where K_e represents exciter gain, T_e exciter time constant. The block uses actual terminal voltage, desired value of terminal voltage and outputs appropriate field voltage to be applied to synchronous alternator. For simulation of PMSG, the excitation is kept constant at 1.0 p.u. in this model of synchronous generator.

C. Wind turbine modeling

This block implements a wind energy conversion system. The inputs are actual and desired speed and the output of the block is mechanical power (P_ω).

The amount of power harnessed from the wind of velocity v is as follows.

$$P_\omega = 1/2 \rho A C_p v^3$$

Where

P_ω = wind power in watts

ρ = air density in kg/m^3

A = swept area in m^2

C_p = power coefficient of wind turbine

v = wind speed in m/s

D. Modeling of control scheme

The control scheme is mainly used to derive reference source currents, which are used in PWM current controller. These are derived in following section.

The reference source currents are having two components, in-phase component and a quadrature component. They are estimated in sequence as follows:

The unit vectors in-phase with v_a , v_b and v_c are derived as:

$$u_a = v_a / V_m; u_b = v_b / V_m; u_c = v_c / V_m \quad (15)$$

Where V_m is the amplitude of the AC terminal voltage at the PCC and can be computed as:

$$V_m = 2/3 \sqrt{(v_a^2 + v_b^2 + v_c^2)} \quad (16)$$

Where v_a , v_b , and v_c are the instantaneous voltages at PCC and can be calculated as:

$$v_a = v_{san} - R_s i_{sa} - L_s p i_{sa} \quad (17)$$

$$v_b = v_{sbn} - R_s i_{sb} - L_s p i_{sb} \quad (18)$$

$$v_c = v_{scn} - R_s i_{sc} - L_s p i_{sc} \quad (19)$$

Where L_s and R_s are per phase source inductance and resistance respectively. V_{san} , v_{sbn} , and v_{scn} are the three phase instantaneous input supply voltages at PCC and are expressed as:

$$v_{san} = v_{sm} \sin(\omega t); v_{sbn} = v_{sm} \sin(\omega t - 2\pi/3); v_{scn} = v_{sm} \sin(\omega t + 2\pi/3) \quad (20)$$



Where v_{sm} is the peak value and $\omega = 2\pi f$ is the frequency of the supply.

The unit vectors in-quadrature with v_a , v_b and v_c may be derived by taking a quadrature transformation of the in-phase unit vectors u_a , u_b and u_c as:

$$w_a = -u_b/\sqrt{3} + u_c/\sqrt{3} \quad (21)$$

$$w_b = \sqrt{3} u_a/2 + (u_b - u_c)/(2\sqrt{3}) \quad (22)$$

$$w_c = -\sqrt{3} u_a/2 + (u_b - u_c)/(2\sqrt{3}) \quad (23)$$

The quadrature component of the reference source currents is computed as:

The voltage error V_{er} at PCC at the n th sampling instant is as:

$$V_{er(n)} = V_{ref(n)} - V_{m(n)} \quad (24)$$

The output of the PI controller at the n th sampling instant is expressed as:

$$I_{smq(n)}^* = I_{smq(n-1)}^* + K_p \{ V_{er(n)} - V_{er(n-1)} \} + K_i V_{er(n)} \quad (25)$$

Where K_p and K_i are the proportional and integral constants, respectively of the proportional integral (PI) controller and the superscript represents the reference quantity.

The quadrature components of the reference source currents are estimates as:

$$I_{saq}^* = I_{smq}^* w_a; i_{sbq}^* = I_{smq}^* w_b; i_{scq}^* = I_{smq}^* w_c \quad (26)$$

The in-phase component of the reference source currents is computed as:

$$I_{sad}^* = I_{smd}^* u_a; i_{sbd}^* = I_{smd}^* u_b; i_{scd}^* = I_{smd}^* u_c \quad (27)$$

Where I_{smd}^* is considered fixed value corresponding to the constant source current for load leveling.

Reference source currents are computed as the sum of the in-phase components of the reference source currents and the quadrature components of the reference source currents given as:

$$I_{sa}^* = i_{saq}^* + i_{sad}^*; i_{sb}^* = i_{sbq}^* + i_{sbd}^*; i_{sc}^* = i_{scq}^* + i_{scd}^* \quad (28)$$

These source reference currents are compared with the sensed source currents in PWM current controller. The current errors of all the three phases are amplified. If the amplified reference source current error signal, i_{saerr} , is greater than the triangular wave carrier signal, switch S_1 is ON and switch S_4 is OFF, and the value of SA is 1. When the amplified reference source current error signal is less than the triangular wave carrier signal switch S_1 is OFF and switch S_4 is ON, and the value of SA is 0. Similar logic applies to other phases.

8. SIMULATION RESULTS

The Figures, 8-11 show the voltages on inverter side (V_{abc_inv}), currents on inverter side (I_{abc_inv}), voltage at point of common coupling (PCC) (V_{pcc}), current at PCC (I_{pcc}), grid voltages (V_{grid}), Grid currents (I_{grid}) and the DC-link voltage (V_{dc}). The rating of the PMSG is given in the Appendix.

A. Performance of the PMSG based AC-DC-AC conversion system during healthy conditions

The wind driven PMSG is run at 94 rpm. The out voltage is 150 V at 60 hertz. This variable voltage and variable frequency output is converted to constant voltage and constant frequency source. The Figure-8 shows the performance of the PMSG during healthy conditions.

B. Performance of the PMSG based AC-DC-AC conversion system during balanced fault conditions

A balanced three-phase symmetrical fault on the load bus was simulated at 1.0 seconds. The fault was cleared at 1.14 seconds. Thus voltage sag of 140 ms was simulated. During the fault condition the proposed system stay connected to the local grid feeding active and reactive power. Figure-9 shows the performance of PMSG during symmetrical fault conditions.

C. Performance of the PMSG based AC-DC-AC conversion system during unbalanced fault conditions

An unsymmetrical fault (phase to phase and phase to ground) on the load bus was simulated at 1.0 seconds. The fault was cleared at 1.14 seconds. Thus voltage sag of 140 ms was simulated. During the fault condition the proposed system stay connected to the local grid feeding active and reactive power. Figures, 10&11 shows the performance of PMSG during unsymmetrical fault conditions.

9. CONCLUSIONS

In this paper a new topology has been proposed for grid connection during symmetrical and unsymmetrical fault conditions to enhance the variable speed driven PMSG fed AC-DC-AC system fault ride-through capability. The proposed technology is simulated in MATLAB using powersim toolbox. The effects of symmetrical and unsymmetrical fault are investigated in a case study. Simulation results prove that the proposed control strategy is able to provide full ride through to the generator. In the case of symmetrical and unsymmetrical fault conditions in grid network the ac voltage of PCC can meet the basic requirements of grid network concerning voltage. On the other hand according to simulation results variable speed driven PMSG is not significantly impacted in abnormal conditions. So it can remain connecting to the grid during and after grid short circuit fault. The inverter is controlled so as to meet IEEE standard 1547 requirements for connection of distributed generation to the local grid. The simulated results validate the proposed topology.

Appendix

Permanent Magnet Synchronous Generator 3-Phase, 300 V, 60 Hz, 3000 rpm, 4-pole

Electromagnetic torque:	0.8 Nm
Stator resistance (R_s):	18.7 Ω
Inductance: LD (H) = Lq (H):	0.02682 H
Flux induce by magnets:	0.1717 wb

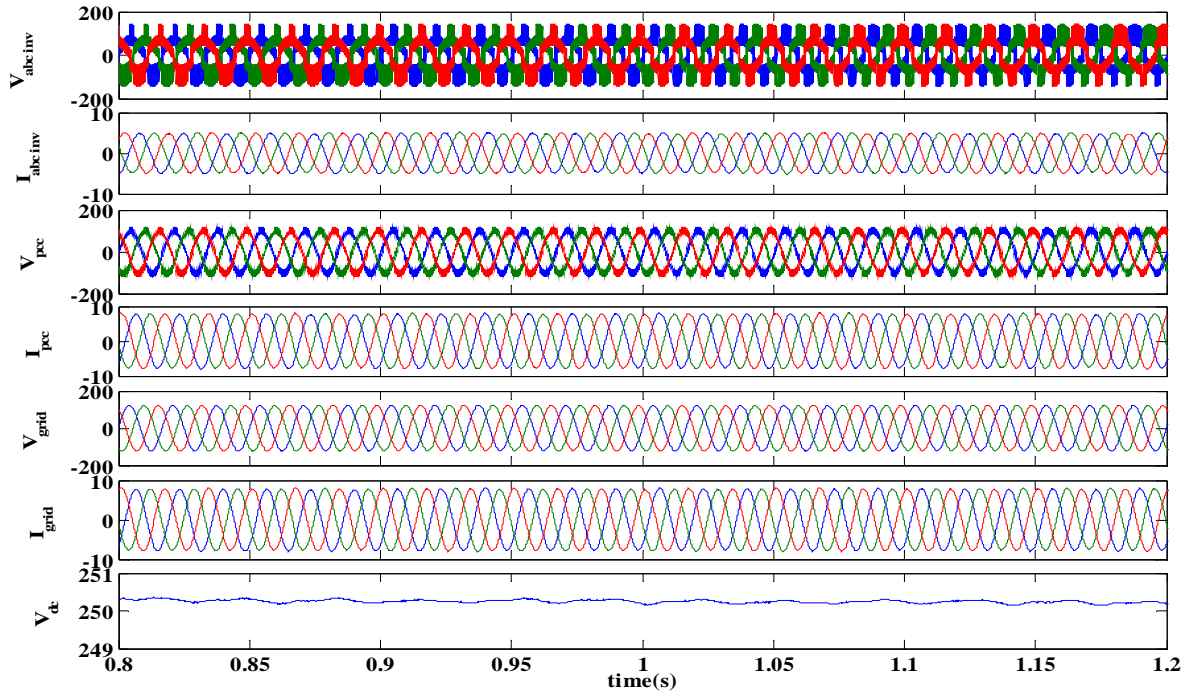


Figure-8. Variation of inverter voltages, currents, during healthy operation.

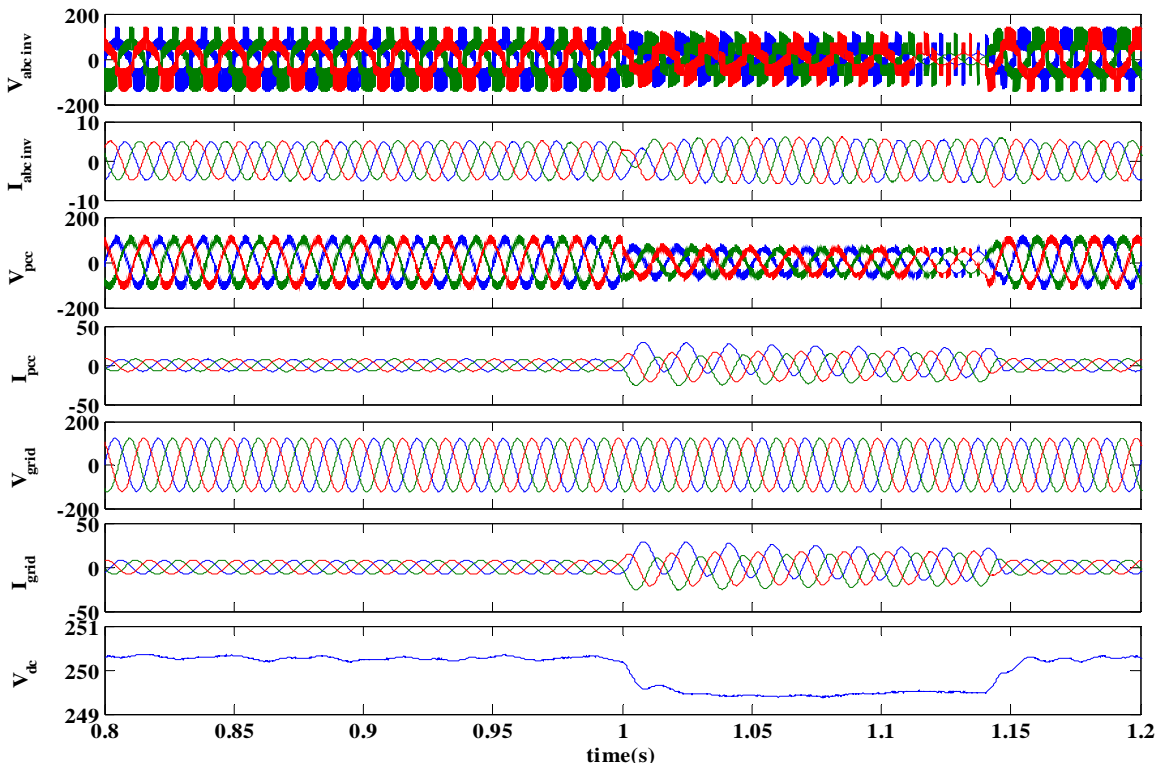


Figure-9. Variation of inverter voltages, currents, during symmetrical fault ride-through of PMSG.

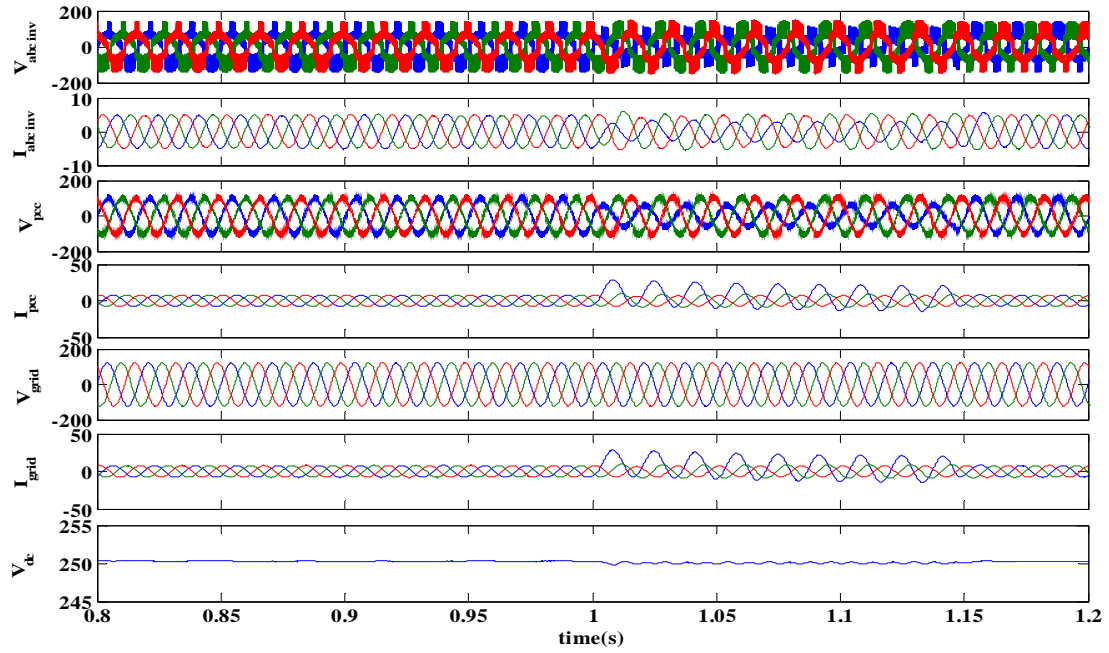


Figure-10. Variation of inverter voltages, currents, during unsymmetrical (phase to ground) fault ride-through of PMSG.

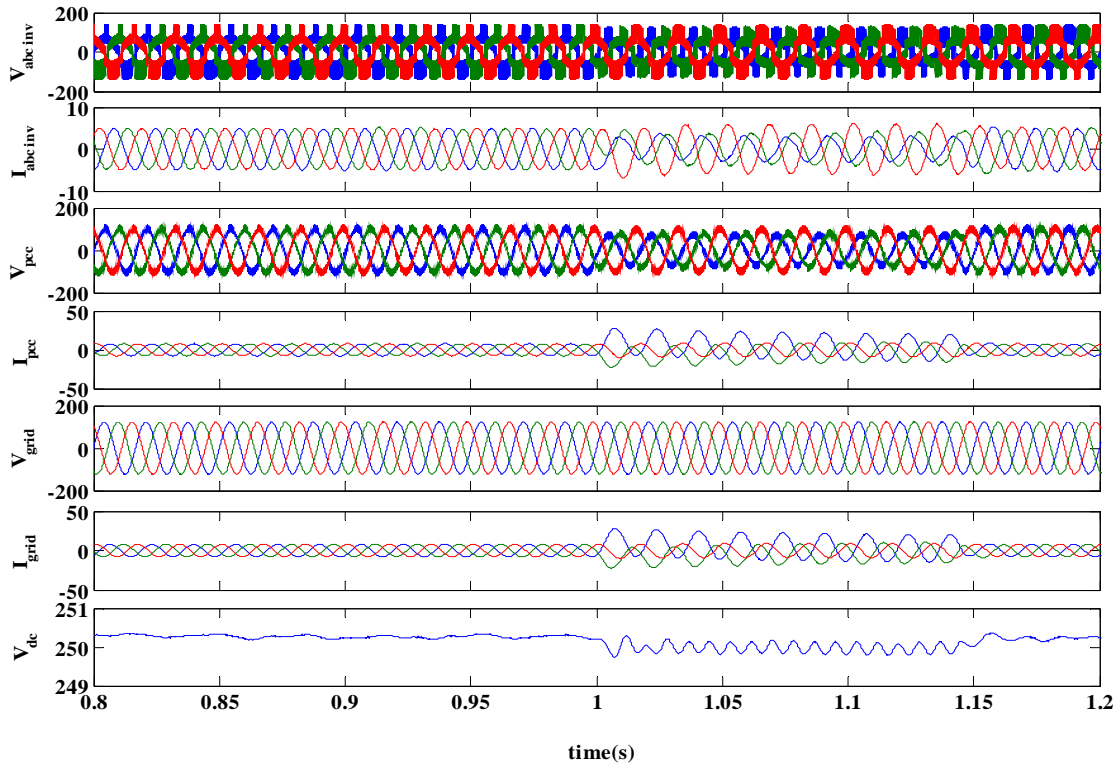


Figure-11. Variation of inverter voltages, currents, during unsymmetrical (phase to phase) fault ride-through of PMSG.



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